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# Benzotriazol-1-yl methyl ferrocene-1,1'dicarboxylate

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Key indicators: single-crystal X-ray study; T = 173 K; mean  $\sigma$ (C–C) = 0.003 Å; R factor = 0.038; wR factor = 0.096; data-to-parameter ratio = 14.1.

The title compound,  $CH_3O-C(O)-Fc-C(O)-OBt$  or  $[Fe(C_7H_7O_2)(C_{12}H_8N_3O_2)]$  (Bt is benzotriazole), shows a *cis* configuration of the Bt group relative to the ferrocene core, with the benzene ring in close proximity to the methyl ester group.

#### **Related literature**

For related literature, see: Heinze & Schlenker (2004); Kraatz et al. (1997); Mahmoud et al. (2005); Taylor & Kennard (1982).



#### **Experimental**

#### Crystal data

 $[Fe(C_7H_7O_2)(C_{12}H_8N_3O_2)]$   $M_r = 405.19$ Monoclinic,  $P2_1/c$  a = 8.2720 (3) Å b = 10.9180 (3) Å c = 18.7460 (5) Å  $\beta = 91.383$  (2)°

#### Data collection

Bruker–Nonius KappaCCD diffractometer Absorption correction: multi-scan (SCALEPACK; Otwinowski & Minor, 1997)  $T_{\rm min} = 0.837, T_{\rm max} = 0.889$ 

#### Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.038$  $wR(F^2) = 0.096$ S = 1.053460 reflections  $V = 1692.53 (9) Å^{3}$ Z = 4 Mo K\alpha radiation \(\mu = 0.92 mm^{-1}\) T = 173 (2) K 0.20 \times 0.20 \times 0.13 mm

12048 measured reflections 3460 independent reflections 2801 reflections with  $I > 2\sigma(I)$  $R_{\text{int}} = 0.060$ 

245 parameters H-atom parameters constrained 
$$\begin{split} &\Delta \rho_{max}=0.31\ e\ {\mbox{\AA}}^{-3}\\ &\Delta \rho_{min}=-0.47\ e\ {\mbox{\AA}}^{-3} \end{split}$$

Data collection: *COLLECT* (Nonius, 1998); cell refinement: *HKL DENZO* and *SCALEPACK* (Otwinowski & Minor, 1997); data reduction: *HKL DENZO* and *SCALEPACK*; program(s) used to solve structure: *SIR97* (Altomare *et al.*, 1999); program(s) used to refine structure: *SHELXL97* (Sheldrick, 1997); molecular graphics: *ORTEP* in *SHELXTL-NT* (Bruker, 2003); software used to prepare material for publication: *WinGX* (Version 1.70.01; Farrugia, 1999).

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: IM2012).

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### Benzotriazol-1-yl methyl ferrocene-1,1'-dicarboxylate

### H.-B. Kraatz, G. Schatte and A. Lataifeh

#### Comment

The ferrocene ester of 1-hydroxybenzotriazole (HOBt) is useful in the preparation of ferrocene peptide conjugates (Kraatz *et al.*, 1997; Mahmoud *et al.*, 2005). The reactivity of Fc-OBt ester towards external nucleophiles is attributed to the increasing electrophilicity of the carbonyl carbon upon esterfication, driven by the lack of interaction between the Cp and OBt  $\pi$ -systems (Mahmoud *et al.*, 2005). Compound (1) crystalizes in the monoclinic space group  $P2_1/c$ . The two cyclopentadienyl groups of the ferrocence moiety are in the eclipsed conformation with a Cp—Fe—Cp angle 177.8 (6)°. The two ester groups are in the 1,2' conformation around the ferrocene center, they are almost coplanar to the Cp rings with torsion angles for C(14)—C10)—C(15)—O(12) and C(24)—C(20)—C(25)—O(22) of 1.1 (3)° and -0.3 (3)°, respectively, unlike to those found in Fc—C(O)-OBt (10.06 (10)°; Kraatz *et al.*, 1997) and Boc-N(H)—Fc—C(O)-OBt (5.0 (7)°; Mahmoud *et al.*, 2005). The benzotriazole moiety is perpendicular with respect to the Cp it is attached to [C(15)—O(12)—N(11)—C(16)] = 87.0 (0)°). This type of arrangement is also found in the related compounds with *cis*-configuration relative to ferrocene moiety in Fc—C(O)-OBt (96.56 (6)°; Kraatz *et al.*, 1997), Boc-N(H)—Fc—C(O)-OBt (80.8 (2)°); Mahmoud *et al.*, 2005) and *trans*-configuration in Ac—N(H)—Fc—C(O)-OBt (88.6°) (Heinze *et al.*, 2004). Presumably the weak hydrogen bond interaction between O(21) and C(17)(H) is responsible for the observed conformation in 1, (C=O(21)—C(17)(H) 3.233 Å; sum of the van der waals radii 3.25 Å; Taylor *et al.*, 1982).

#### Experimental

Solid 1-hydroxybenzotriazole (HOBt) (4.40 mmol, 0.67 g) and 1-Ethyl-3-(3-dimethylaminopropyl)carbodiimide hydrochloride (EDC·HCl) (4.40 mmol, 0.84 g) were added to a solution of 1'-(methoxycarbonyl)-ferrocene-1-carboxylic acid (3.93 mmol, 0.80 g) in CH<sub>2</sub>Cl<sub>2</sub> (50 ml). The reaction mixture was stirred for 2 h at room temperature, and then washed with aqueous solutions of saturated sodium bicarbonate (NaHCO<sub>3</sub>), citric acid, and water. The organic phase was separated and dried with anhydrous Na<sub>2</sub>SO<sub>4</sub>, then filtered and the solvent CH<sub>2</sub>Cl<sub>2</sub> evaporated under reduced pressure. The crude product was purified by flash chromatography (SiO<sub>2</sub>,  $R_f$ = 0.55, EtOAc/hexane, 1:2) to give dark orange crystals of (Benzotriazole-1-yl)-1'-(methoxycarbonyl)-ferrocene-1- carboxylate (1) (2.38 mmol, 0.9678 g, yield: 61%).

Suitable crystals of (1) for X-ray diffraction were obtained by slow diffusion (layering technique) of *n*-hexane into a solution of (1) in  $CH_2Cl_2$ . Dark orange crystals were obtained after 24 h. An orange squared-like crystal of (1) was coated with oil (Paratone 8277, Exxon), was collected onto the nylon fiber of a mounted CryoLoopTM (Hampton Research, USA) under a microscope. The crystal was then mounted onto the goniometer head, which was quickly transferred to the cold stream of the X-ray diffractometer.

#### Refinement

The structure was solved using direct methods (SIR97) and refined by full-matrix least-squares method on  $F^2$  with SHELXL97–2. The non-hydrogen atoms were refined anisotropically. Hydrogen atoms were included at geometrically ideal-

ized positions (C—H bond distances 0.95/0.98/1.00) and were not refined. The isotropic thermal parameters of the hydrogen atoms were fixed at 1.2 times that of the preceding carbon atom.

## Figures



**Figure 1** *ORTEP* diagram of the molecular structure of (1). Displacement ellipsoids are drawn at the 30% probability level.

### Benzotriazol-1-yl methyl ferrocene-1,1'-dicarboxylate

| Crystal data                       |  |
|------------------------------------|--|
| $[Fe(C_7H_7O_2)(C_{12}H_8N_3O_2)]$ | $F_{000} = 832$                              |
| $M_r = 405.19$                     | $D_{\rm x} = 1.590 {\rm ~Mg} {\rm m}^{-3}$   |
| Monoclinic, $P2_1/c$               | Mo $K\alpha$ radiation $\lambda = 0.71073$ Å |
| Hall symbol: -P 2ybc               | Cell parameters from 3308 reflections        |
| a = 8.2720 (3) Å                   | $\theta = 1.0-27.9^{\circ}$                  |
| b = 10.9180 (3) Å                  | $\mu = 0.92 \text{ mm}^{-1}$                 |
| c = 18.7460 (5)  Å                 | T = 173 (2)  K                               |
| $\beta = 91.383 \ (2)^{\circ}$     | Square, orange                               |
| $V = 1692.53 (9) \text{ Å}^3$      | $0.20\times0.20\times0.13~mm$                |
| Z = 4                              |  |

## Data collection

| Bruker–Nonius KappaCCD<br>diffractometer  | 3460 independent reflections           |
|---|--|
| Radiation source: Nonius FR590D, fine-focus sealed tube                         | 2801 reflections with $I > 2\sigma(I)$ |
| Monochromator: horizonally mounted graphite crystal                             | $R_{\text{int}} = 0.060$               |
| T = 173(2)  K   | $\theta_{\text{max}} = 26.4^{\circ}$   |
| CCD rotation images, thick slices scans   | $\theta_{\min} = 2.9^{\circ}$          |
| Absorption correction: multi-scan<br>(HKL Scalepack; (Otwinowski & Minor, 1997) | $h = -10 \rightarrow 10$               |
| $T_{\min} = 0.837, T_{\max} = 0.889$  | $k = -13 \rightarrow 13$               |
| 12048 measured reflections  | $l = -23 \rightarrow 22$               |

#### Refinement

| Refinement on $F^2$        | Secondary atom site location: difference Fourier map     |
|----------------------------|--|
| Least-squares matrix: full | Hydrogen site location: inferred from neighbouring sites |

 $R[F^{2} > 2\sigma(F^{2})] = 0.038$ H-atom parameters constrained  $wR(F^{2}) = 0.096$   $WR(F^{2}) = 0.096$   $Where P = (F_{o}^{2} + 2F_{c}^{2})/3$  S = 1.05  $(\Delta/\sigma)_{max} = 0.001$   $\Delta\rho_{max} = 0.31 \text{ e} \text{ Å}^{-3}$   $\Delta\rho_{min} = -0.47 \text{ e} \text{ Å}^{-3}$ Primary atom site location: structure-invariant direct

Primary atom site location: structure-invariant direct methods Extinction correction: none

#### Special details

**Geometry**. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor *wR* and goodness of fit S are based on  $F^2$ , conventional *R*-factors *R* are based on F, with F set to zero for negative  $F^2$ . The threshold expression of  $F^2 > 2 \text{sigma}(F^2)$  is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$  are statistically about twice as large as those based on F, and R– factors based on ALL data will be even larger.

| = $($ $=$ $)$ $($ $)$ $($ $=$ $)$ $($ $)$ $($ $)$ $($ $)$ $($ $)$ $($ $)$ $($ | Fractional a | atomic | coordinates | and | isotropic d | or equival | ent isotropic | displacemen | t parameters | (Å | 2) |
|---|--------------|--------|-------------|-----|-------------|------------|---------------|-------------|--------------|----|----|
|---|--------------|--------|-------------|-----|-------------|------------|---------------|-------------|--------------|----|----|

|     | x           | у            | Ζ             | $U_{\rm iso}$ */ $U_{\rm eq}$ |
|-----|-------------|--------------|---------------|-------------------------------|
| Fe1 | 0.48612 (4) | 0.32889 (3)  | 0.651633 (18) | 0.01915 (11)                  |
| 011 | 0.3274 (2)  | 0.24087 (16) | 0.46478 (10)  | 0.0306 (4)                    |
| 012 | 0.1545 (2)  | 0.37941 (16) | 0.51327 (9)   | 0.0269 (4)                    |
| O21 | 0.0387 (2)  | 0.30425 (16) | 0.68935 (10)  | 0.0301 (4)                    |
| O22 | 0.1579 (2)  | 0.43584 (16) | 0.76631 (9)   | 0.0288 (4)                    |
| N11 | 0.0386 (3)  | 0.32276 (19) | 0.47099 (11)  | 0.0268 (5)                    |
| N12 | 0.0142 (3)  | 0.3614 (2)   | 0.40315 (12)  | 0.0331 (5)                    |
| N13 | -0.0968 (3) | 0.2906 (2)   | 0.37430 (12)  | 0.0313 (5)                    |
| C10 | 0.4275 (3)  | 0.3847 (2)   | 0.55082 (13)  | 0.0215 (5)                    |
| C11 | 0.5928 (3)  | 0.3463 (2)   | 0.55495 (14)  | 0.0243 (5)                    |
| H11 | 0.6395      | 0.2819       | 0.5283        | 0.029*                        |
| C12 | 0.6745 (3)  | 0.4212 (2)   | 0.60574 (14)  | 0.0278 (6)                    |
| H12 | 0.7858      | 0.4160       | 0.6191        | 0.033*                        |
| C13 | 0.5608 (3)  | 0.5061 (2)   | 0.63342 (14)  | 0.0276 (6)                    |
| H13 | 0.5838      | 0.5673       | 0.6683        | 0.033*                        |
| C14 | 0.4077 (3)  | 0.4839 (2)   | 0.60019 (13)  | 0.0241 (5)                    |
| H14 | 0.3102      | 0.5267       | 0.6090        | 0.029*                        |
| C15 | 0.3077 (3)  | 0.3240 (2)   | 0.50473 (13)  | 0.0222 (5)                    |
| C16 | -0.0509 (3) | 0.2232 (2)   | 0.48724 (13)  | 0.0207 (5)                    |
| C17 | -0.0671 (3) | 0.1509 (2)   | 0.54821 (13)  | 0.0234 (5)                    |
| H17 | -0.0060     | 0.1659       | 0.5909        | 0.028*                        |
| C18 | -0.1770 (3) | 0.0568 (2)   | 0.54249 (13)  | 0.0256 (5)                    |
| H18 | -0.1903     | 0.0033       | 0.5819        | 0.031*                        |
| C19 | -0.2711 (3) | 0.0377 (2)   | 0.47938 (14)  | 0.0269 (5)                    |
|     |             |              |               |                               |

| H19  | -0.3470     | -0.0276    | 0.4778       | 0.032*     |
|------|-------------|------------|--------------|------------|
| C20  | 0.3148 (3)  | 0.2773 (2) | 0.72174 (12) | 0.0220 (5) |
| C21  | 0.3525 (3)  | 0.1773 (2) | 0.67550 (13) | 0.0233 (5) |
| H21  | 0.2788      | 0.1359     | 0.6442       | 0.028*     |
| C22  | 0.5201 (3)  | 0.1511 (2) | 0.68493 (14) | 0.0284 (6) |
| H22  | 0.5779      | 0.0890     | 0.6609       | 0.034*     |
| C23  | 0.5864 (3)  | 0.2336 (3) | 0.73637 (14) | 0.0317 (6) |
| H23  | 0.6960      | 0.2359     | 0.7527       | 0.038*     |
| C24  | 0.4609 (3)  | 0.3119 (2) | 0.75923 (13) | 0.0272 (6) |
| H24  | 0.4717      | 0.3759     | 0.7933       | 0.033*     |
| C25  | 0.1567 (3)  | 0.3375 (2) | 0.72331 (12) | 0.0211 (5) |
| C26  | 0.0080 (4)  | 0.5040 (3) | 0.76726 (15) | 0.0345 (6) |
| H26A | -0.0236     | 0.5276     | 0.7185       | 0.041*     |
| H26B | 0.0229      | 0.5778     | 0.7965       | 0.041*     |
| H26C | -0.0768     | 0.4529     | 0.7875       | 0.041*     |
| C110 | -0.2558 (3) | 0.1102 (2) | 0.42076 (14) | 0.0270 (6) |
| H110 | -0.3208     | 0.0974     | 0.3790       | 0.032*     |
| C111 | -0.1408 (3) | 0.2044 (2) | 0.42423 (13) | 0.0233 (5) |
|      |             |            |              |            |

# Atomic displacement parameters $(\text{\AA}^2)$

|      | $U^{11}$     | U <sup>22</sup> | $U^{33}$     | $U^{12}$     | $U^{13}$      | $U^{23}$     |
|------|--------------|-----------------|--------------|--------------|---------------|--------------|
| Fe1  | 0.01780 (19) | 0.01764 (18)    | 0.02191 (19) | 0.00037 (13) | -0.00146 (13) | 0.00061 (13) |
| 011  | 0.0315 (11)  | 0.0281 (10)     | 0.0320 (10)  | -0.0011 (8)  | -0.0020 (8)   | -0.0040 (8)  |
| 012  | 0.0203 (9)   | 0.0268 (9)      | 0.0333 (10)  | -0.0017 (7)  | -0.0065 (7)   | -0.0018 (8)  |
| O21  | 0.0234 (10)  | 0.0329 (10)     | 0.0339 (10)  | -0.0006 (8)  | -0.0027 (8)   | -0.0069 (8)  |
| O22  | 0.0311 (10)  | 0.0283 (9)      | 0.0270 (9)   | 0.0061 (8)   | -0.0019 (7)   | -0.0103 (8)  |
| N11  | 0.0212 (11)  | 0.0313 (11)     | 0.0274 (11)  | -0.0044 (9)  | -0.0084 (9)   | 0.0039 (9)   |
| N12  | 0.0286 (13)  | 0.0399 (13)     | 0.0306 (12)  | -0.0005 (10) | -0.0040 (10)  | 0.0100 (10)  |
| N13  | 0.0284 (12)  | 0.0359 (12)     | 0.0294 (12)  | -0.0022 (10) | -0.0074 (10)  | 0.0063 (10)  |
| C10  | 0.0206 (13)  | 0.0194 (11)     | 0.0245 (12)  | -0.0008 (9)  | 0.0011 (10)   | 0.0044 (9)   |
| C11  | 0.0197 (12)  | 0.0255 (12)     | 0.0276 (13)  | 0.0006 (10)  | 0.0018 (10)   | 0.0020 (10)  |
| C12  | 0.0173 (12)  | 0.0329 (14)     | 0.0331 (14)  | -0.0062 (10) | -0.0015 (10)  | 0.0045 (11)  |
| C13  | 0.0304 (14)  | 0.0191 (12)     | 0.0333 (14)  | -0.0063 (10) | -0.0022 (11)  | -0.0007 (10) |
| C14  | 0.0232 (13)  | 0.0184 (11)     | 0.0309 (13)  | 0.0008 (10)  | 0.0030 (10)   | 0.0052 (10)  |
| C15  | 0.0214 (13)  | 0.0216 (12)     | 0.0237 (12)  | 0.0007 (10)  | 0.0016 (10)   | 0.0068 (10)  |
| C16  | 0.0159 (11)  | 0.0226 (12)     | 0.0234 (12)  | 0.0017 (9)   | -0.0007 (9)   | -0.0012 (10) |
| C17  | 0.0195 (12)  | 0.0296 (13)     | 0.0210 (12)  | 0.0038 (10)  | -0.0019 (10)  | 0.0007 (10)  |
| C18  | 0.0235 (13)  | 0.0256 (12)     | 0.0279 (13)  | 0.0052 (10)  | 0.0047 (10)   | 0.0024 (10)  |
| C19  | 0.0217 (13)  | 0.0238 (12)     | 0.0352 (14)  | -0.0014 (10) | 0.0002 (10)   | -0.0049 (11) |
| C20  | 0.0295 (14)  | 0.0190 (11)     | 0.0174 (11)  | -0.0014 (10) | -0.0013 (10)  | 0.0007 (9)   |
| C21  | 0.0272 (13)  | 0.0177 (11)     | 0.0251 (12)  | -0.0021 (10) | 0.0025 (10)   | 0.0005 (10)  |
| C22  | 0.0319 (15)  | 0.0213 (12)     | 0.0322 (14)  | 0.0075 (10)  | 0.0045 (11)   | 0.0058 (10)  |
| C23  | 0.0270 (14)  | 0.0379 (15)     | 0.0299 (14)  | 0.0044 (11)  | -0.0054 (11)  | 0.0089 (12)  |
| C24  | 0.0291 (14)  | 0.0307 (14)     | 0.0215 (12)  | 0.0015 (11)  | -0.0067 (10)  | -0.0012 (10) |
| C25  | 0.0257 (13)  | 0.0204 (11)     | 0.0171 (11)  | -0.0029 (10) | 0.0017 (10)   | 0.0006 (9)   |
| C26  | 0.0395 (16)  | 0.0336 (14)     | 0.0307 (14)  | 0.0123 (12)  | 0.0055 (12)   | -0.0017 (12) |
| C110 | 0.0219 (13)  | 0.0274 (13)     | 0.0312 (13)  | 0.0024 (10)  | -0.0088 (11)  | -0.0076 (11) |

| C111            | 0.0207 (12)   | 0.0269 (12) | 0.0221 (12) | 0.0038 (10) | -0.0034 (10) | -0.0017 (10) |
|-----------------|---------------|-------------|-------------|-------------|--------------|--------------|
| Geometric param | neters (Å, °) |             |             |             |              |              |
| Fe1—C10         |               | 2.033 (2)   | C13–        | C14         | 1.4          | 19 (4)       |
| Fe1—C20         |               | 2.035(2)    | C13-        | -H13        | 0.9          | 500          |
| Fe1—C24         |               | 2.041 (3)   | C14-        | -H14        | 0.9          | 500          |
| Fe1—C11         |               | 2.044 (3)   | C16–        | -C111       | 1.39         | 96 (3)       |
| Fe1—C14         |               | 2.046 (2)   | C16–        | -C17        | 1.39         | 98 (3)       |
| Fe1—C21         |               | 2.046 (2)   | C17–        | C18         | 1.3          | 75 (4)       |
| Fe1—C22         |               | 2.056 (2)   | C17–        | -H17        | 0.9          | 500          |
| Fe1—C23         |               | 2.057 (3)   | C18–        | C19         | 1.4          | 15 (4)       |
| Fe1—C12         |               | 2.062 (3)   | C18–        | -H18        | 0.9          | 500          |
| Fe1—C13         |               | 2.062 (2)   | C19–        | C110        | 1.30         | 53 (4)       |
| O11—C15         |               | 1.191 (3)   | C19–        | -H19        | 0.93         | 500          |
| O12—N11         |               | 1.376 (3)   | C20–        | -C21        | 1.43         | 33 (3)       |
| O12—C15         |               | 1.416 (3)   | C20–        | C24         | 1.43         | 33 (4)       |
| O21—C25         |               | 1.208 (3)   | C20–        | C25         | 1.40         | 65 (3)       |
| O22—C25         |               | 1.342 (3)   | C21–        | -C22        | 1.42         | 23 (4)       |
| O22—C26         |               | 1.447 (3)   | C21–        | -H21        | 0.93         | 500          |
| N11—N12         |               | 1.350 (3)   | C22–        | C23         | 1.42         | 20 (4)       |
| N11—C16         |               | 1.354 (3)   | C22–        | -H22        | 0.93         | 500          |
| N12—N13         |               | 1.308 (3)   | C23–        | C24         | 1.42         | 20 (4)       |
| N13—C111        |               | 1.382 (3)   | C23–        | -H23        | 0.93         | 500          |
| C10-C11         |               | 1.431 (3)   | C24–        | -H24        | 0.93         | 500          |
| C10-C14         |               | 1.437 (3)   | C26–        | -H26A       | 0.98         | 300          |
| C10-C15         |               | 1.458 (3)   | C26–        | -H26B       | 0.98         | 300          |
| C11—C12         |               | 1.415 (4)   | C26–        | -H26C       | 0.98         | 300          |
| C11—H11         |               | 0.9500      | C110        | —C111       | 1.40         | 01 (4)       |
| C12—C13         |               | 1.427 (4)   | C110        | —H110       | 0.93         | 500          |
| C12—H12         |               | 0.9500      |             |             |              |              |
| C10—Fe1—C20     |               | 121.94 (10) | C14-        |             | 69.          | 16 (13)      |
| C10—Fe1—C24     |               | 156.62 (10) | C12-        | -C13-Fe1    | 69.7         | 74 (14)      |
| C20—Fe1—C24     |               | 41.17 (10)  | C14-        | -С13—Н13    | 125          | .7           |
| C10—Fe1—C11     |               | 41.09 (9)   | C12–        | -С13—Н13    | 125          | .7           |
| C20—Fe1—C11     |               | 157.02 (10) | Fe1—        | -C13—H13    | 127          | .0           |
| C24—Fe1—C11     |               | 160.29 (11) | C13–        | -C14C10     | 107          | .3 (2)       |
| C10—Fe1—C14     |               | 41.25 (10)  | C13–        | -C14-Fe1    | 70.4         | 43 (14)      |
| C20—Fe1—C14     |               | 108.41 (10) | C10–        | -C14-Fe1    | 68.9         | 91 (13)      |
| C24—Fe1—C14     |               | 120.14 (10) | C13-        | -C14H14     | 126          | .3           |
| C11—Fe1—C14     |               | 69.14 (10)  | C10–        | -C14-H14    | 126          | .3           |
| C10—Fe1—C21     |               | 109.12 (10) | Fe1—        | -C14—H14    | 125          | .9           |
| C20—Fe1—C21     |               | 41.10 (9)   | 011–        | -C15-O12    | 122          | .2 (2)       |
| C24—Fe1—C21     |               | 69.00 (10)  | 011–        | C15C10      | 128          | .1 (2)       |
| C11—Fe1—C21     |               | 121.08 (10) | 012–        | C15C10      | 109          | .7 (2)       |
| C14—Fe1—C21     |               | 127.26 (10) | N11–        | -C16-C111   | 102          | .1 (2)       |
| C10—Fe1—C22     |               | 126.35 (10) | N11–        | -C16-C17    | 134          | .5 (2)       |
| C20—Fe1—C22     |               | 68.58 (10)  | C111-       |             | 123          | .3 (2)       |
| C24—Fe1—C22     |               | 68.34 (10)  | C18–        | -C17-C16    | 115          | .7 (2)       |

| C11—Fe1—C22                     | 107.34 (10)          | C18—C17—H17  | 122.1             |
|---------------------------------|----------------------|--|-------------------|
| C14—Fe1—C22                     | 164.48 (11)          | C16—C17—H17  | 122.1             |
| C21—Fe1—C22                     | 40.59 (10)           | C17—C18—C19  | 121.6 (2)         |
| C10—Fe1—C23                     | 162.20 (10)          | C17—C18—H18  | 119.2             |
| C20—Fe1—C23                     | 68.61 (10)           | C19—C18—H18  | 119.2             |
| C24—Fe1—C23                     | 40.54 (11)           | C110—C19—C18   | 121.9 (2)         |
| C11—Fe1—C23                     | 123.85 (11)          | С110—С19—Н19   | 119.0             |
| C14—Fe1—C23                     | 154.17 (11)          | C18—C19—H19  | 119.0             |
| C21—Fe1—C23                     | 68.40 (11)           | C21—C20—C24  | 107.8 (2)         |
| C22—Fe1—C23                     | 40.38 (11)           | C21—C20—C25  | 124.1 (2)         |
| C10—Fe1—C12                     | 68.37 (10)           | C24—C20—C25  | 127.9 (2)         |
| C20—Fe1—C12                     | 161.79 (10)          | C21-C20-Fe1  | 69.86 (14)        |
| C24—Fe1—C12                     | 123.59 (10)          | C24—C20—Fe1  | 69.64 (14)        |
| C11—Fe1—C12                     | 40.32 (10)           | C25—C20—Fe1  | 121.63 (16)       |
| C14—Fe1—C12                     | 68.47 (10)           | C22—C21—C20  | 107.6 (2)         |
| C21—Fe1—C12                     | 154.80 (10)          | C22—C21—Fe1  | 70.09 (14)        |
| C22—Fe1—C12                     | 119.28 (11)          | C20-C21-Fe1  | 69.04 (13)        |
| C23—Fe1—C12                     | 105.95 (11)          | C22—C21—H21  | 126.2             |
| C10—Fe1—C13                     | 68.33 (10)           | C20—C21—H21  | 126.2             |
| C20—Fe1—C13                     | 125.65 (10)          | Fe1—C21—H21  | 126.3             |
| C24—Fe1—C13                     | 106.68 (11)          | C23—C22—C21  | 108.4 (2)         |
| C11—Fe1—C13                     | 68.19 (10)           | C23—C22—Fe1  | 69.83 (15)        |
| C14—Fe1—C13                     | 40.41 (10)           | C21—C22—Fe1  | 69.32 (13)        |
| C21—Fe1—C13                     | 163.93 (10)          | C23—C22—H22  | 125.8             |
| C22—Fe1—C13                     | 153.73 (11)          | C21—C22—H22  | 125.8             |
| C23—Fe1—C13                     | 119.06 (11)          | Fe1—C22—H22  | 126.6             |
| C12—Fe1—C13                     | 40 49 (11)           | $C_{22} - C_{23} - C_{24}$   | 1083(2)           |
| N11-012-C15                     | 110.85 (18)          | $C^{22}$ $C^{23}$ $E^{21}$   | 69 78 (15)        |
| $C_{25} = 0^{22} = C_{26}^{26}$ | 115.1.(2)            | $C_24$ — $C_23$ —Fe1   | 69 13 (14)        |
| N12—N11—C16                     | 113.1 (2)            | $C_{22} = C_{23} = H_{23}$   | 125.9             |
| N12—N11—012                     | 119.2 (2)            | $C_{24}$ $C_{23}$ $H_{23}$   | 125.9             |
| C16 - N11 - O12                 | 127 5 (2)            | Fe1_C23_H23  | 126.8             |
| N13_N12_N11                     | 127.5(2)<br>107.0(2) | $C^{23}$ $C^{24}$ $C^{20}$   | 120.0<br>107.9(2) |
| N12 N13 C111                    | 107.0(2)<br>108.4(2) | $C_{23} = C_{24} = C_{20}$   | 107.9(2)          |
| $C_{11} = C_{10} = C_{14}$      | 108.4(2)<br>108.0(2) | $C_{23} - C_{24} - I_{C1}$   | 60 10 (14)        |
| $C_{11} = C_{10} = C_{14}$      | 100.0(2)<br>122.2(2) | $C_{20} = C_{24} = P_{C1}$   | 126.1             |
| $C_{11} = C_{10} = C_{15}$      | 122.5(2)<br>120.6(2) | $C_{23} = C_{24} = H_{24}$   | 120.1             |
| $C_{14} = C_{10} = C_{13}$      | 129.0(2)             | $C_{20} - C_{24} - H_{24}$   | 120.1             |
| C14 $C10$ Fel                   | 69.80(14)            | $re1 - C_2 - T_2 - T_2 - C_2 - T_2 - C_2 $ | 120.0             |
| C14C10Fe1                       | 09.84(14)            | 021 - 025 - 022  | 123.3(2)          |
|                                 | 125.94 (10)          | 021 - C23 - C20  | 124.4 (2)         |
|                                 | 107.9 (2)            | 022 - C25 - C20  | 112.1 (2)         |
| Cl2—Cl1—Fel                     | /0.52 (15)           | 022 - C26 - H26A   | 109.5             |
| Clo—Cl1—Fel                     | 69.05 (14)<br>12( 0  | 022—C26—H26B   | 109.5             |
| C12—C11—H11                     | 126.0                | $H_{20}A - C_{20} - H_{20}B$   | 109.5             |
| CIU—CII—HII                     | 126.0                | U22—U26—H26C   | 109.5             |
| rei—CII—HII                     | 126.0                | H26A—C26—H26C  | 109.5             |
| C11—C12—C13                     | 108.2 (2)            | H26B—C26—H26C  | 109.5             |
| C11—C12—Fe1                     | 69.16 (14)           | C19—C110—C111  | 117.7 (2)         |
| C13—C12—Fe1                     | 69.77 (14)           | C19—C110—H110  | 121.1             |

| C11—C12—H12      | 125.9        | C111—C110—H110   | 121.1        |
|------------------|--------------|------------------|--------------|
| C13—C12—H12      | 125.9        | N13—C111—C16     | 109.3 (2)    |
| Fe1—C12—H12      | 126.7        | N13-C111-C110    | 131.1 (2)    |
| C14—C13—C12      | 108.6 (2)    | C16—C111—C110    | 119.6 (2)    |
| C15—O12—N11—N12  | -87.7 (3)    | C16-C17-C18-C19  | -2.0 (4)     |
| C15—O12—N11—C16  | 87.0 (3)     | C17—C18—C19—C110 | 1.0 (4)      |
| C16—N11—N12—N13  | 2.4 (3)      | C10—Fe1—C20—C21  | 82.68 (17)   |
| O12—N11—N12—N13  | 177.9 (2)    | C24—Fe1—C20—C21  | -118.9 (2)   |
| N11—N12—N13—C111 | -1.2 (3)     | C11—Fe1—C20—C21  | 46.3 (3)     |
| C20—Fe1—C10—C11  | -159.35 (14) | C14—Fe1—C20—C21  | 126.10 (15)  |
| C24—Fe1—C10—C11  | 163.1 (2)    | C22—Fe1—C20—C21  | -37.71 (15)  |
| C14—Fe1—C10—C11  | 119.1 (2)    | C23—Fe1—C20—C21  | -81.23 (16)  |
| C21—Fe1—C10—C11  | -115.71 (15) | C12—Fe1—C20—C21  | -157.0 (3)   |
| C22—Fe1—C10—C11  | -73.68 (18)  | C13—Fe1—C20—C21  | 167.61 (15)  |
| C23—Fe1—C10—C11  | -37.0 (4)    | C10—Fe1—C20—C24  | -158.47 (14) |
| C12—Fe1—C10—C11  | 37.51 (14)   | C11—Fe1—C20—C24  | 165.1 (2)    |
| C13—Fe1—C10—C11  | 81.22 (15)   | C14—Fe1—C20—C24  | -115.04 (15) |
| C20—Fe1—C10—C14  | 81.57 (16)   | C21—Fe1—C20—C24  | 118.9 (2)    |
| C24—Fe1—C10—C14  | 44.1 (3)     | C22—Fe1—C20—C24  | 81.15 (16)   |
| C11—Fe1—C10—C14  | -119.1 (2)   | C23—Fe1—C20—C24  | 37.63 (15)   |
| C21—Fe1—C10—C14  | 125.21 (14)  | C12—Fe1—C20—C24  | -38.1 (4)    |
| C22—Fe1—C10—C14  | 167.24 (15)  | C13—Fe1—C20—C24  | -73.54 (18)  |
| C23—Fe1—C10—C14  | -156.0 (3)   | C10—Fe1—C20—C25  | -35.8 (2)    |
| C12—Fe1—C10—C14  | -81.57 (15)  | C24—Fe1—C20—C25  | 122.7 (2)    |
| C13—Fe1—C10—C14  | -37.86 (14)  | C11—Fe1—C20—C25  | -72.2 (3)    |
| C20—Fe1—C10—C15  | -43.3 (2)    | C14—Fe1—C20—C25  | 7.7 (2)      |
| C24—Fe1—C10—C15  | -80.8 (3)    | C21—Fe1—C20—C25  | -118.4 (3)   |
| C11—Fe1—C10—C15  | 116.0 (3)    | C22—Fe1—C20—C25  | -156.1 (2)   |
| C14—Fe1—C10—C15  | -124.9 (3)   | C23—Fe1—C20—C25  | 160.3 (2)    |
| C21—Fe1—C10—C15  | 0.3 (2)      | C12—Fe1—C20—C25  | 84.6 (4)     |
| C22—Fe1—C10—C15  | 42.4 (3)     | C13—Fe1—C20—C25  | 49.2 (2)     |
| C23—Fe1—C10—C15  | 79.1 (4)     | C24—C20—C21—C22  | 0.1 (3)      |
| C12—Fe1—C10—C15  | 153.6 (2)    | C25—C20—C21—C22  | 174.9 (2)    |
| C13—Fe1—C10—C15  | -162.7(2)    | Fe1—C20—C21—C22  | 59.70 (17)   |
| C14—C10—C11—C12  | -0.4 (3)     | C24—C20—C21—Fe1  | -59.56 (17)  |
| C15—C10—C11—C12  | -178.2 (2)   | C25-C20-C21-Fe1  | 115.2 (2)    |
| Fe1-C10-C11-C12  | -60.06 (17)  | C10—Fe1—C21—C22  | 124.03 (15)  |
| C14—C10—C11—Fe1  | 59.64 (16)   | C20—Fe1—C21—C22  | -118.9 (2)   |
| C15-C10-C11-Fe1  | -118.2 (2)   | C24—Fe1—C21—C22  | -80.81 (16)  |
| C10—Fe1—C11—C12  | 119.0 (2)    | C11—Fe1—C21—C22  | 80.28 (17)   |
| C20—Fe1—C11—C12  | 169.0 (2)    | C14—Fe1—C21—C22  | 166.62 (15)  |
| C24—Fe1—C11—C12  | -41.1 (4)    | C23—Fe1—C21—C22  | -37.16 (15)  |
| C14—Fe1—C11—C12  | 80.92 (16)   | C12—Fe1—C21—C22  | 44.4 (3)     |
| C21—Fe1—C11—C12  | -157.29 (15) | C13—Fe1—C21—C22  | -158.0 (3)   |
| C22—Fe1—C11—C12  | -115.08 (16) | C10—Fe1—C21—C20  | -117.03 (15) |
| C23—Fe1—C11—C12  | -73.80 (18)  | C24—Fe1—C21—C20  | 38.14 (15)   |
| C13—Fe1—C11—C12  | 37.40 (15)   | C11—Fe1—C21—C20  | -160.77 (14) |
| C20—Fe1—C11—C10  | 50.0 (3)     | C14—Fe1—C21—C20  | -74.43 (17)  |
| C24—Fe1—C11—C10  | -160.0 (3)   | C22—Fe1—C21—C20  | 118.9 (2)    |
|                  | × /          |                  |              |

| C14—Fe1—C11—C10                              | -38.07(14)             | C23—Fe1—C21—C20                         | 81.79 (16)             |
|--|------------------------|---|------------------------|
| C21—Fe1—C11—C10                              | 83.72 (16)             | C12—Fe1—C21—C20                         | 163.3 (2)              |
| C22—Fe1—C11—C10                              | 125.93 (15)            | C13—Fe1—C21—C20                         | -39.1 (4)              |
| $C_{23}$ —Fe1—C11—C10                        | 167.21 (14)            | $C_{20}$ $C_{21}$ $C_{22}$ $C_{23}$     | 0.0 (3)                |
| C12—Fe1—C11—C10                              | -119.0(2)              | Fe1—C21—C22—C23                         | 59.05 (18)             |
| C13—Fe1—C11—C10                              | -81.59 (15)            | C20—C21—C22—Fe1                         | -59.04 (16)            |
| C10-C11-C12-C13                              | 0.1 (3)                | C10—Fe1—C22—C23                         | 163.61 (15)            |
| Fe1—C11—C12—C13                              | -59.05 (18)            | C20—Fe1—C22—C23                         | -81.75 (16)            |
| C10-C11-C12-Fe1                              | 59.14 (17)             | C24—Fe1—C22—C23                         | -37.33 (16)            |
| C10—Fe1—C12—C11                              | -38.20 (14)            | C11—Fe1—C22—C23                         | 122.25 (16)            |
| C20—Fe1—C12—C11                              | -166.2(3)              | C14—Fe1—C22—C23                         | -163.4 (3)             |
| C24—Fe1—C12—C11                              | 164.58 (14)            | C21—Fe1—C22—C23                         | -119.9 (2)             |
| C14—Fe1—C12—C11                              | -82.72 (16)            | C12—Fe1—C22—C23                         | 80.04 (18)             |
| $C_{21}$ —Fe1—C12—C11                        | 50.9 (3)               | C13—Fe1—C22—C23                         | 46.5 (3)               |
| $C_{22}$ —Fe1—C12—C11                        | 82.38 (17)             | C10 - Fe1 - C22 - C21                   | -7647(18)              |
| $C_{23}$ —Fe1—C12—C11                        | 123 96 (15)            | $C_{20}$ Fe1 - $C_{22}$ - $C_{21}$      | 38 17 (14)             |
| C13 - Fe1 - C12 - C11                        | -1197(2)               | $C_{24}$ Fe1 $C_{22}$ $C_{21}$          | 82 59 (16)             |
| C10 - Fe1 - C12 - C13                        | 81 52 (16)             | $C_{11}$ $F_{e1}$ $C_{22}$ $C_{21}$     | -117.83(15)            |
| $C_{20}$ Fe1 $C_{12}$ $C_{13}$               | -465(4)                | C14—Fe1—C22—C21                         | -43 5 (4)              |
| $C_{24}$ Fe1 $C_{12}$ $C_{13}$               | $-75\ 70\ (18)$        | $C_{23}$ Fe1 $C_{22}$ $C_{21}$          | 119.9 (2)              |
| $C_{11}$ $F_{e1}$ $C_{12}$ $C_{13}$          | 119.7 (2)              | C12—Fe1— $C22$ — $C21$                  | -160.04(14)            |
| $C_{14}$ $F_{e1}$ $C_{12}$ $C_{13}$          | 37.01 (15)             | C12 - Fc1 - C22 - C21                   | 166.5(2)               |
| $C_{1} = C_{1} = C_{12} = C_{13}$            | 170.7 (2)              | $C_{13} = C_{12} = C_{23} = C_{24}$     | -0.2(3)                |
| $C_{22}$ $E_{e1}$ $C_{12}$ $C_{13}$          | -157.90(16)            | $E_{21} - C_{22} - C_{23} - C_{24}$     | 5857(18)               |
| $C_{22}$ — $C_{12}$ — $C_{13}$               | -116 32 (16)           | $C_{21} = C_{22} = C_{23} = C_{24}$     | -58.73(17)             |
| $C_{23}$ $C_{12}$ $C_{12}$ $C_{13}$ $C_{14}$ | 0.3(3)                 | $C_{21} - C_{22} - C_{23} - C_{10}$     | -480(4)                |
| $C_{11} - C_{12} - C_{13} - C_{14}$          | -58.39(17)             | $C_{10} = C_{10} = C_{23} = C_{22}$     | 40.0 (4)<br>81.67 (16) |
| $C_{11} = C_{12} = C_{13} = C_{14}$          | 58 68 (18)             | $C_{20} = C_{10} = C_{23} = C_{22}$     | (10)                   |
| $C_{11} - C_{12} - C_{13} - F_{61}$          | 38.00(10)              | $C_{24} = Fe_{1} = C_{23} = C_{22}$     | -76.42(10)             |
| $C_{10}$ $-re_{1}$ $C_{13}$ $C_{14}$         | -75.04(18)             | C11 - Fe1 - C23 - C22                   | -70.42(19)             |
| $C_{20}$ Fe1 $C_{13}$ $C_{14}$               | -73.94(18)             | $C_{14} = Fe_{1} = C_{23} = C_{22}$     | 109.9(2)               |
| $C_{24}$ $-re_{1}$ $-C_{13}$ $-C_{14}$       | -11/.1/(10)            | $C_{21}$ — $re_1$ — $C_{23}$ — $C_{22}$ | 37.34 (13)             |
| C11 - Fe1 - C13 - C14                        | 83.02 (16)             | C12 - Fe1 - C23 - C22                   | -110.08 (10)           |
| $C_{21}$ —Fe1—C13—C14                        | -45.5(4)               | C13 - Fe1 - C23 - C22                   | -158.45(10)            |
| $C_{22}$ FeI $C_{13}$ $C_{14}$               | 108.1(2)<br>150.24(15) | C10—Fe1— $C23$ — $C24$                  | -10/.9(3)              |
| $C_{23}$ —FeI—CI3—CI4                        | -139.34(15)            | $C_{20}$ —FeI— $C_{23}$ — $C_{24}$      | -38.20(15)             |
| C12—FeI—C13—C14                              | 120.3 (2)              | C11 - Fe1 - C23 - C24                   | 163.70(15)             |
| C10—FeI— $C13$ — $C12$                       | -81.64(16)             | C14—Fe1— $C23$ — $C24$                  | 50.0 (3)               |
| $C_{20}$ —FeI—CI3—CI2                        | 163.80 (14)            | $C_{21}$ —Fe1— $C_{23}$ — $C_{24}$      | -82.54 (17)            |
| $C_24$ —FeI—CI3—CI2                          | 122.57 (16)            | $C_{22}$ —FeI— $C_{23}$ — $C_{24}$      | -119.9 (2)             |
| CII - FeI - CI3 - CI2                        | -37.25 (15)            | C12—Fe1— $C23$ — $C24$                  | 123.44 (16)            |
| C14—Fe1—C13—C12                              | -120.3 (2)             | C13—Fe1—C23—C24                         | 81.69 (18)             |
| $C_21$ —FeI—CI3—CI2                          | -165.5 (3)             | $C_{22} - C_{23} - C_{24} - C_{20}$     | 0.2 (3)                |
| C22—FeI—C13—C12                              | 4/.8 (3)               | FeI—C23—C24—C20                         | 59.22 (17)             |
| $C_{23} - FeI - CI_{3} - CI_{2}$             | 80.39 (17)             | C22—C23—C24—Fel                         | -58.97 (18)            |
| C12—C13—C14—C10                              | -0.5 (3)               | C21—C20—C24—C23                         | -0.2 (3)               |
| FeI—C13—C14—C10                              | -59.28 (16)            | C25—C20—C24—C23                         | -174.8 (2)             |
| C12—C13—C14—Fe1                              | 58.74 (18)             | Fe1—C20—C24—C23                         | -59.93 (18)            |
| C11—C10—C14—C13                              | 0.6 (3)                | C21—C20—C24—Fe1                         | 59.70 (17)             |
| C15-C10-C14-C13                              | 178.2 (2)              | C25—C20—C24—Fe1                         | -114.8 (2)             |

| Fe1-C10-C14-C13  | 60.25 (17)   | C10—Fe1—C24—C23   | 170.7 (2)    |
|------------------|--------------|-------------------|--------------|
| C11-C10-C14-Fe1  | -59.65 (16)  | C20—Fe1—C24—C23   | 119.0 (2)    |
| C15-C10-C14-Fe1  | 117.9 (3)    | C11—Fe1—C24—C23   | -43.7 (4)    |
| C10—Fe1—C14—C13  | -118.4 (2)   | C14—Fe1—C24—C23   | -157.28 (16) |
| C20—Fe1—C14—C13  | 123.83 (15)  | C21—Fe1—C24—C23   | 80.91 (17)   |
| C24—Fe1—C14—C13  | 80.22 (18)   | C22—Fe1—C24—C23   | 37.19 (17)   |
| C11—Fe1—C14—C13  | -80.46 (16)  | C12—Fe1—C24—C23   | -74.39 (19)  |
| C21—Fe1—C14—C13  | 165.70 (15)  | C13—Fe1—C24—C23   | -115.46 (17) |
| C22—Fe1—C14—C13  | -160.1 (3)   | C10—Fe1—C24—C20   | 51.7 (3)     |
| C23—Fe1—C14—C13  | 45.1 (3)     | C11—Fe1—C24—C20   | -162.7 (3)   |
| C12—Fe1—C14—C13  | -37.08 (15)  | C14—Fe1—C24—C20   | 83.73 (16)   |
| C20—Fe1—C14—C10  | -117.79 (14) | C21—Fe1—C24—C20   | -38.08 (14)  |
| C24—Fe1—C14—C10  | -161.39 (14) | C22—Fe1—C24—C20   | -81.80 (16)  |
| C11—Fe1—C14—C10  | 37.93 (14)   | C23—Fe1—C24—C20   | -119.0 (2)   |
| C21—Fe1—C14—C10  | -75.92 (17)  | C12—Fe1—C24—C20   | 166.62 (14)  |
| C22—Fe1—C14—C10  | -41.7 (4)    | C13—Fe1—C24—C20   | 125.56 (15)  |
| C23—Fe1—C14—C10  | 163.4 (2)    | C26—O22—C25—O21   | -2.5 (3)     |
| C12—Fe1—C14—C10  | 81.31 (15)   | C26—O22—C25—C20   | 176.6 (2)    |
| C13—Fe1—C14—C10  | 118.4 (2)    | C21—C20—C25—O21   | 5.1 (4)      |
| N11-012-C15-011  | 1.0 (3)      | C24—C20—C25—O21   | 178.8 (2)    |
| N11-012-C15-C10  | -179.20 (18) | Fe1—C20—C25—O21   | 91.0 (3)     |
| C11-C10-C15-O11  | -1.8 (4)     | C21—C20—C25—O22   | -174.0 (2)   |
| C14—C10—C15—O11  | -179.1 (2)   | C24—C20—C25—O22   | -0.3 (3)     |
| Fe1-C10-C15-O11  | -88.1 (3)    | Fe1—C20—C25—O22   | -88.0 (2)    |
| C11-C10-C15-O12  | 178.4 (2)    | C18—C19—C110—C111 | 1.1 (4)      |
| C14—C10—C15—O12  | 1.1 (3)      | N12-N13-C111-C16  | -0.3 (3)     |
| Fe1-C10-C15-O12  | 92.1 (2)     | N12-N13-C111-C110 | 178.5 (3)    |
| N12—N11—C16—C111 | -2.5 (3)     | N11-C16-C111-N13  | 1.6 (3)      |
| O12-N11-C16-C111 | -177.5 (2)   | C17-C16-C111-N13  | 179.9 (2)    |
| N12—N11—C16—C17  | 179.5 (3)    | N11-C16-C111-C110 | -177.3 (2)   |
| O12-N11-C16-C17  | 4.5 (5)      | C17—C16—C111—C110 | 1.0 (4)      |
| N11—C16—C17—C18  | 178.7 (3)    | C19—C110—C111—N13 | 179.3 (3)    |
| C111—C16—C17—C18 | 1.0 (4)      | C19—C110—C111—C16 | -2.0 (4)     |



